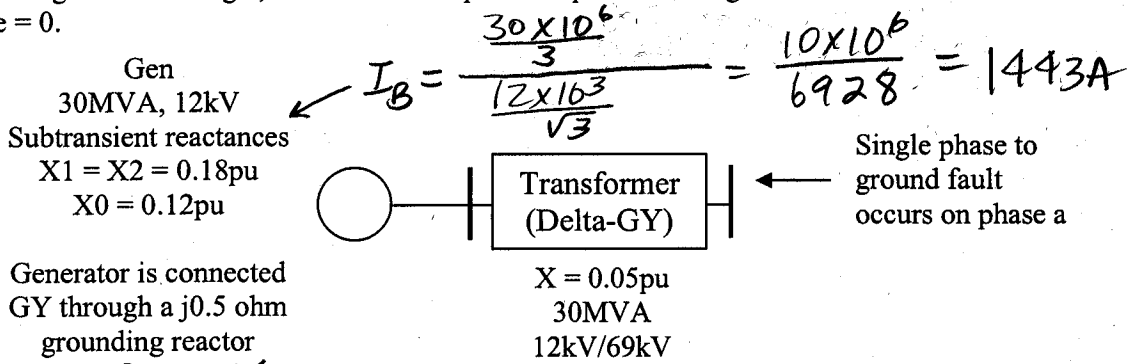


A 30MVA, 12kV generator is connected to a delta - grounded wye transformer. The generator and transformer are isolated and not connected to a "power grid." Impedances are given on equipment bases.

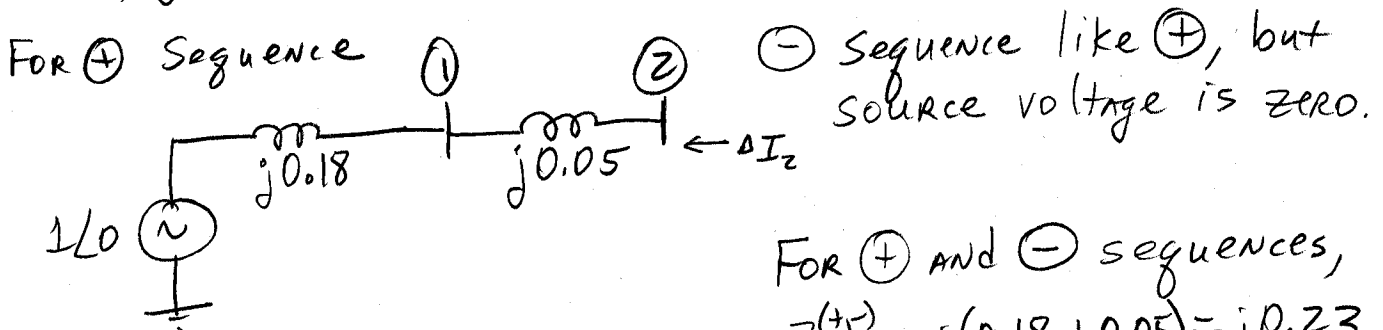
A single-phase to ground fault, with zero impedance, suddenly appears on phase a of the 69kV transformer terminal. Find the resulting a-b-c generator currents (magnitude in amperes and phase). Regarding reference angle, assume that the pre-fault phase a voltage on the transformer's 69kV bus has angle = 0.



Generator is connected GY through a j0.5 ohm grounding reactor

$$Z_B = \frac{(12)^2}{30} = \frac{144}{30} = 4.8 \Omega$$

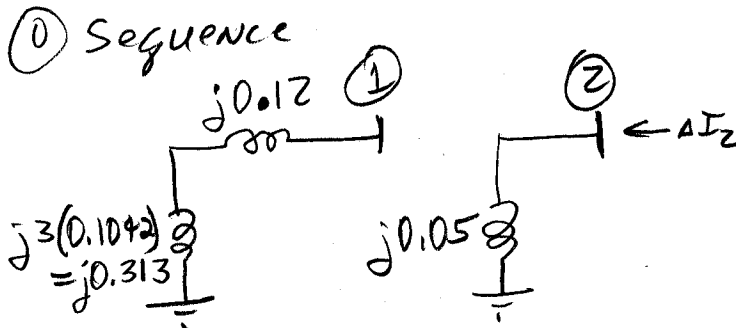
$$\text{So, } j0.5 \Omega = j0.1042 \text{ pu}$$



For \oplus and \ominus sequences,

$$Z_{22}^{(+)} = j(0.18 + 0.05) = j0.23$$

$$Z_{12}^{(+)} = \frac{2V_1}{jI_2} = \frac{j0.18 I_2}{I_2} = j0.18$$



For \odot sequence

$$Z_{22}^{(0)} = j0.05, \quad Z_{12}^{(0)} = 0$$

Now, for the fault current,

$$I_{za}^F = \frac{3V_{za}^{pre}}{Z_{22}^{(0)} + Z_{22}^{(1)} + Z_{22}^{(2)} + 3Z_{12}^{(0)}} = \frac{3\angle 0}{j0.05 + 2j(0.23)} = -j5.88 \text{ pu}$$

For a single phase fault, we know that

$$I_{k0}^F = I_{k1}^F = I_{k2}^F = \frac{1}{3} I_{ka}^F, \quad \text{So } I_{2,0}^F = I_{2,1}^F = I_{2,2}^F = \frac{-j5.88}{3} = -j1.96 \text{ pu}$$

Test 9, 11/5/04, continued

Now, \oplus and \ominus sequence currents are the same at the generator (except for phase shift) because we have a simple series path. Furthermore, the zero sequence current does not flow through the transformer. Thus, on the generator side, we have

$$I_{gen,1}^F = -j1.960 \left(1 \angle -30^\circ \right) = 1.960 \angle -120^\circ$$

$$I_{gen,2}^F = -j1.960 \left(1 \angle +30^\circ \right) = 1.960 \angle -60^\circ$$

$$I_{gen,0}^F = 0.$$

Converting to abc

$$\begin{bmatrix} I_a \\ I_b \\ I_c \end{bmatrix} = \begin{bmatrix} 1 & 1 & 1 \\ 1 & a^2 & a \\ 1 & a & a^2 \end{bmatrix} \begin{bmatrix} 0 \\ 1.960 \angle -120^\circ \\ 1.960 \angle -60^\circ \end{bmatrix} = \begin{bmatrix} 1.960 \angle -120^\circ + 1.960 \angle -60^\circ \\ 1.960 \angle 120^\circ + 1.960 \angle 60^\circ \\ 1.960 \angle 0^\circ + 1.960 \angle -180^\circ \end{bmatrix}$$

$$\begin{bmatrix} I_a \\ I_b \\ I_c \end{bmatrix} = 1.960 \begin{bmatrix} 1 \angle -120^\circ + 1 \angle -60^\circ \\ 1 \angle 120^\circ + 1 \angle 60^\circ \\ 0 \end{bmatrix} = 1.960 \begin{bmatrix} \sqrt{3} \angle -90^\circ \\ \sqrt{3} \angle 90^\circ \\ 0 \end{bmatrix}$$

$$\begin{bmatrix} I_a \\ I_b \\ I_c \end{bmatrix} = \begin{bmatrix} -j3.39 \\ j3.39 \\ 0 \end{bmatrix}. \text{ IN AMPS, } \begin{bmatrix} I_a \\ I_b \\ I_c \end{bmatrix} = \begin{bmatrix} -j4892 \\ j4892 \\ 0 \end{bmatrix}$$

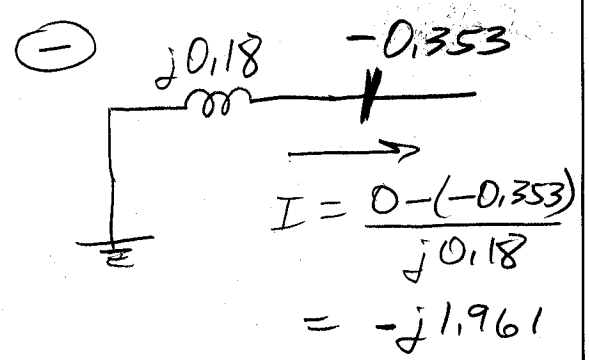
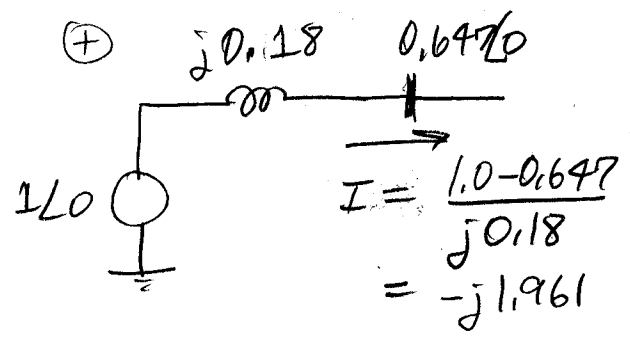
Note — in the general case, you use the off-diagonal z elements. Doing the problem in the way ...

$$V_{1,0}^F = \cancel{V_{1,0}^{pre}} - \cancel{Z_{12,0}} I_{2,0}^F = 0$$

$$V_{1,1}^F = V_{1,1}^{pre} - Z_{13,1} I_{3,1}^F = 1.0 - j0.18(-j1.960) = 1.0 - 0.353 = 0.647$$

$$V_{1,2}^F = \cancel{V_{1,2}^{pre}} - Z_{13,2} I_{3,2}^F = -j0.18(-j1.960) = -0.353$$

Then, using the network



You can see these currents match the previous ones. And so on,